

1 **Restructuring of emergent grain boundaries at free surfaces – an interplay** 2 **between core stabilization and elastic stress generation**

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16 **Abstract**

17 Scanning tunneling microscopy and calculations are used to study the structure and relaxation
18 of grain boundaries at the surface of planar nanocrystalline copper (111) films and
19 bicrystals. We show that the strong energetic preference for boundary cores to lie along close-
20 packed planes introduces a restructuring that rotates adjoining grains and generates elastic
21 stresses in the triple junction region. The interplay of this stress field and the core stabilization
22 determines the length scale of the restructuring and controls the shape and magnitude of the
23 displacement field around the triple junction. Depending on the in-plane angle, restructured
24 boundaries can extend to depths of ~ 15 nm with the associated elastic stress fields extending
25 to even greater depths. These results point to a new mechanism of boundary relaxation at
26 surfaces that is expected to be important in grain coalescence, film stress evolution and the
27 properties of nanoscale materials.

28 **Main**

29 **Introduction**

30 Grain boundaries (GBs) impact a wide range of properties – electrical transport in nanoscale
31 materials ¹, intergranular corrosion and catalysis at surface ²⁻⁵, stress evolution in thin films ^{6,7},
32 and the mechanical strength of polycrystalline materials ⁸ – all critical to materials and device
33 technologies ⁹⁻¹². The ever-increasing demand for innovation has heightened the need for an
34 improved understanding of GBs and their impact on performance ¹³⁻¹⁵. However, little is
35 known about the atomic-scale behavior of emergent grain boundaries (eGBs) at the surfaces of
36 macroscopic materials. These studies are particularly challenging due to surface corrosion
37 phenomena and the potential of capping layers used in TEM to suppress the intrinsic behavior
38 of eGBs. Thus, it is challenging for TEM to detect atomic relaxation along the axis of eGBs
39 or the natural shape of the triple junction (TJ) so that the eGB behavior and their associated
40 surface and size effects have largely gone unstudied experimentally ^{16,17}. Alternatively, the
41 structure of eGBs is known to control dynamical thermal grooving at high temperatures ¹⁸⁻²⁰,
42 but is poorly understood at lower temperatures where structure and stress play important roles.

43 Here we studied the structure of eGBs on surfaces of copper (111) nanocrystalline films and
 44 bicrystals, using of UHV cryogenic STM together with numerical calculations. The picometer
 45 resolution of STM allows a precise mapping of the atomic structure of eGBs and the
 46 displacement field of the free surface at the TJ. We identify the existence of a restructuring
 47 phenomenon that is driven by an energetic preference for boundary cores to lie along close-
 48 packed planes (CPPs) that involves the rotation of adjoining grains and the generation of elastic
 49 stresses in the TJ region. The interplay of the core stabilization and this stress field determines
 50 the length scale of the restructured boundary and controls the shape and magnitude of the
 51 displacement field around the TJ.

52 *Atomic & nanoscale structures and geometrical analysis*

53 We begin by considering the atomic structure of an eGB on a 50 nm thick nanocrystalline
 54 copper (111) film. Details of the sample, preparation and STM measurement are provided in
 55 the Supplementary Material (SM). Figure 1a shows the perspective view of the TJ, where the
 56 boundary meets the surface. The grains on either side of the boundary are about 20 nm wide
 57 and TJ is located in a local groove. Fig. 1b shows an atomic resolution image of this boundary.
 58 Both sides are clearly (111) surfaces as expected and eGB cores show dislocation-like features
 59 similar to the emergent LAGB previously reported²¹. Although the atomic planes are curved
 60 or rotated downwards into the GB plane, there is no evidence of step formation, consistent with
 61 a free surface that is able to respond to the presence of a stress field in the subsurface region.
 62 The absence of surface steps confirms that the groove is not related to the Mullins' thermal-
 63 grooving phenomenon and Wulff construction^{18,19,22}.

64 The misorientation or in-plane angle θ measured in Fig. 1b between the $[1\bar{1}0]$ directions
 65 of the two adjoining grains is $\sim 25^\circ$. In the half period of the boundary, the Burgers circuit in
 66 green shows that there is a $\bar{B}/2 = [1\bar{1}0]$ closure failure along half of the period vector $\bar{p}/2 =$
 67 $5/4 [\bar{1}\bar{1}2] + 2/4 [1\bar{1}0]$, one with a spacing $3/4 [\bar{1}\bar{1}2] + 1/4 [1\bar{1}0]$ and another with a
 68 spacing $2/4 [\bar{1}\bar{1}2] + 1/4 [1\bar{1}0]$. When inserted into Frank's formula²³

$$69 \quad \sin(\theta/2) = B/2p \quad [1]$$

70 we find $\theta = 26.01^\circ$, which agrees well with our measurement of $\sim 25^\circ$. Hence, we will refer
 71 to this boundary as eGB26. Using the surface basis of $1/4 [\bar{1}\bar{1}2]$ and $1/4 [1\bar{1}0]$, the period
 72 vector can be rewritten as $[10,4]$ in surface notation, which decomposes into
 73 $[10,4]=[3,1]+[2,1]+[3,1]+[2,1]$ or $[3,2,3,2]$ for short.

74 The nature of the restructured boundary is evident from an analysis of the displacement
 75 field around the TJ. The groove width and minimum depth measured across the local maxima
 76 along the TJ are ~ 3 nm and ~ 65 pm, respectively (Fig 1c) and groove volume is ~ 16 atoms
 77 per period. Away from the boundary on either side of the groove the grains recover and return
 78 towards the planar orientation. The local angle within the groove is ~ 0.15 rad or $\sim 8.6^\circ$,
 79 meaning that the atomic planes on either side of the boundary are rotated 4.3° away from the
 80 film normal. The global angle beyond the TJ groove is $\sim 0.7^\circ$. Previously we showed that
 81 adjoining grains at low angle boundaries in nanocrystalline copper (111) films exhibit an out-
 82 of-plane rotation angle φ that scales with the in-plane misorientation angle θ :
 83 $\tan(\varphi/2) = 1/2\sqrt{2} \cdot \sin(\theta/2)$ ²¹. The driving force for out-of-plane rotation is the energy
 84 anisotropy of the dislocation line that favors a $[112]$ tilt axis that stabilizes the GB cores by
 85 enabling them to lie long $\{111\}$ planes. For eGB26, the predicted rotation angle $\varphi/2$ on each
 86 side of the boundary is $\sim 4.5^\circ$ and very close to the local 4.3° groove angle measured in Fig.
 87 1c, d. From the boundary geometry perspective²¹, a finite local groove angle implies that close
 88 to the surface the local tilt axis is shifted away from $[111]$ towards $[112]$, whereas the constant
 89 near-zero angle ($\sim 0.7^\circ$) further away from the boundary implies that deep into the film the tilt

90 axis returns to [111]. Different tilt axis have different symmetry, which indicates a phase-like
91 restructuring around the TJ. We tested the generality of these results by mapping the TJ
92 displacement field for a wide range of GB angles and found excellent agreement between the
93 local groove angle and that predicted by the $(\theta/2, \varphi/2)$ scaling (see Fig. 1d). As expected, a
94 finite positive (negative) global angle results in a smaller (larger) local angle compared to that
95 predicted by geometry. Collectively, these results point to a strong preference for GB cores to
96 lie along {111} planes regardless of the GB misorientation angle (see below).

97 ***Bicrystal & surface effect***

98 To further confirm the generality of these results and that the shift of the tilt axis towards
99 [112] is a property of eGBs in copper [111] materials, we employed STM to analyze the
100 structure of the single boundary in an engineered macroscopic bicrystal. The bicrystal was 2
101 mm thick and 8 mm diameter and comprised of two Cu (111) single crystals that have been
102 oriented and fused to form a GB 26.01° boundary (MaTeck Material). The preparation of the
103 bicrystal for STM analysis is described in SM.

104 Figure 2a shows the presence of the single boundary and the arrangement of surface steps
105 on either side of this boundary. A close-up view image is shown in Fig. 2b, which was recorded
106 at a location >10 nm from the nearest step. Figure 2b inset shows an atomic resolution image
107 of the adjoining crystals of the bicrystal that confirms the (111) surface periodicity and that the
108 in-plane angle is indeed 26.01 degrees. Importantly we note the period vector of the boundary
109 decomposes into [3,2,3,2], identical to the decomposition observed in nanocrystalline film in
110 Fig. 1b. The displacement field across the bicrystal boundary is shown in Fig. 2c. The TJ exists
111 within a groove formed between the adjoining crystals. Topographic-sections across the groove
112 recorded under different bias conditions (see Fig. SM-1) show evidence of an electronic effect
113 at larger positive bias (also seen in nanocrystalline films), the width and depth of the groove is
114 essentially identical to that recorded for the nanocrystalline film. The local angle is 5.1° while
115 far from the groove the global angle is $\sim -0.5^\circ$. The existence of near identical eGBs at the
116 surfaces of 50 nm thick nanocrystalline films and macroscopic bicrystals demonstrates that the
117 restructured eGB26 is not influenced by the limited grain size (~ 50 nm) in the film and that the
118 length scale of restructured boundary is much smaller than this grain size.

119 ***Bulk GB energy calculation***

120 STM provides a direct measurement of TJ structure and the displacement normal to the
121 surface. To understand the boundary restructuring and associated subsurface deformation
122 fields, we rely on numerical calculations. Since for LAGBs the shift of the tilt axis towards
123 [112] leads to a reduction of the boundary energy²¹, we calculated the corresponding driving
124 force for a wide range of in-plane angles, i.e., the energy difference $\Delta\gamma$ between a bulk GB
125 with a tilt axis [111] and its corresponding bulk boundary with the tilt axis shifted toward [112],
126 shown schematically as black and red in Fig. SM-2, respectively (GB geometrical
127 specifications in SM). Classical molecular statics (MS) calculation results in Fig. 3a show that
128 for all in-plane angles θ , the [112] tilt boundary is always lower in energy. For each in-plane
129 angle, the boundary energy decreases smoothly as the tilt axis shifts across the range of possible
130 tilt axes between [111] and [112], revealing the absence of a thermodynamic barrier to grain
131 rotation. For copper, the values of $\Delta\gamma$ range from 70 mJ m^{-2} to 300 mJ m^{-2} depending on the
132 misorientation angle θ and in all instances $\Delta\gamma$ is a significant fraction of the original boundary
133 energy. For GB 26.01° , $\Delta\gamma = 112 \text{ mJ/m}^2$, or $\sim 14\%$ of the GB 26.01° energy of 833 mJ/m^2
134 (see Fig. SM-3).

135 ***eGB calculation***

136 To see if the reduction in the bulk GB energy results in GB restructuring at the surface, we
 137 perform all-atom MS and molecular dynamics (MD) simulations of the symmetric tilt eGB26
 138 in an $H \geq 50$ nm thick [111] copper film (SM and Tab. SM-1). While we observe a narrower
 139 and shallower groove compared to experiment (depth < 10 pm and full width at half maximum
 140 (FWHM) < 1 nm) at a [3,2,3,2] decomposed surface TJ, the structural transition of the boundary
 141 is absent (Figure SM-4). The change in energy of the TJ in the eGB26 is negligible
 142 (Supplementary Note and Fig. SM-7). Alternatively, mechanical reorientation of the rotated
 143 eGB[112]26 onto a (111) substrate preserves the [112] misorientation axis and the TJ
 144 structure (see Fig. SM-6). While the eGB energy now increases due to the (elastic) stresses
 145 associated with the reorientation, the surface profiles show increasing agreement with the
 146 experimental profiles (Fig. 1c & 2c) as the thickness of the reoriented eGB[112]26 is decreased
 147 to below 10 nm (Fig. SM-8). This is suggestive of partial rotation of the top layer and is
 148 consistent with a simple dimensional analysis: for a reoriented film of total height H , the elastic
 149 energy cost scales as volume ($\sim H^2$) while the GB energy reduction is proportional to its area
 150 ($\sim H\Delta\gamma$).

151 We study the stability of the partially rotated eGB system using a modified computational
 152 framework eGB system summarized in Fig. 3b (see SM). The rotation is now limited to a top
 153 layer of varying thickness h and consisting of a V-shaped notch with an included angle φ .
 154 Commensurability between the rotated and reference (unrotated) regions of the film is ensured
 155 by shear-stitching the notch along the boundary normal, resulting in a valley at the eGB.
 156 Analogously, shear-packing of the cutout wedge at the eGBs leads to ridges at the GBs that
 157 bound the cell edges. The shear stitching/packing scheme is equivalent to the rotation of the
 158 top layer to eliminate the notch/wedge and mate it with the rest of the crystal, as summarized
 159 in Fig. SM-9.

160 *eGB subsurface structure*

161 Figure 4a shows the atomic-scale TJ structure following an equilibrium MS simulation of
 162 a $h = 1.25$ nm [6 (111) layers] thick rotated layer within an $H = 50$ nm thick film. The
 163 corrugation along the groove is evident from the surface profiles extracted at local maxima and
 164 minima, labelled X1 and X2 respectively. The corresponding line profiles plotted in Fig. 4b
 165 reveal groove depths of $D1 \approx 100$ pm and $D2 \approx 40$ pm respectively, and a surface width
 166 (FWHM ~ 1.5 nm) that is at least 50% larger compared to the unrotated eGB and similar to
 167 experimental FWHM of 1.3 nm. The local angle at the minima is $\sim \varphi$ and the global angle
 168 asymptotes to zero over a ~ 10 nm width centered at the eGB (Fig. 4b). The periodic TJ
 169 structure shows the emergence of dislocation-like features with a decomposition consistent
 170 with experiments (top, Fig. 4c). Subsurface characterization reveals co-existence of the two
 171 distinct GB structures with a transition at approximately the prescribed layer thickness h
 172 (bottom, Fig. 4c). This restructured eGB is stable to preparing temperatures (~ 800 K). Varying
 173 h at fixed film thickness ($H = 50$ nm) leads to similar groove profiles, albeit with differing TJ
 174 widths (Fig. SM-10). The energy of each of these partially rotated eGBs is lower than that of
 175 the rotated and reoriented film, indicating that the equilibrium top layer thickness is less than
 176 50 nm, consistent with the size independent local groove angles observed in the experiments.

177 *eGB energetics: driving force for eGB restructuring and its stability*

178 We analyze the stability of the partially rotated eGB system using a combination of scaling
 179 analyses and continuum computations. For a (111) copper film with surface energy γ_s , the
 180 driving force for rotation (per film width) to form a valley is (Supplementary Note)

$$181 \quad \Delta U_F = [\gamma_{[112]}/\cos(\varphi/2) - \gamma_{[111]}]h - [2\gamma_s \cdot \tan(\varphi/2)]h \quad [2]$$

182 where the first term is the contribution from the reduction in the GB area and the second term
 183 is the surface area eliminated by shear-stitching the notch ¹. The elastic deformation energy
 184 scales quadratically with the notch height h and shear strain φ . Detailed finite element method
 185 (FEM) computations of a shear-stitched surface notch (see SM) reveal a top layer under tension
 186 (Fig. SM-11) and a net elastic energy of the form

$$187 \quad \Delta U_e = f(h/H) C(v) G (\varphi h)^2 \quad [3]$$

188 where G is the shear modulus, C is a material constant set by the Poisson's ratio ν , and the
 189 function f is the correction due to the finite thickness of the film parametrized by the ratio h/H
 190 (Fig. SM-12 and Supplementary Note).

191 Figure 4d shows the layer thickness dependence of these energetic contributions for the
 192 eGB26 system with film thickness $H = 50$ nm. The relevant interfacial and bulk parameters
 193 for pure copper are listed in Tab. SM-3~5. The elastic energy curve is plotted as a range based
 194 on anisotropy in the elastic parameters of pure copper (G, ν) along and normal to the film,
 195 including the average over all orientations in a randomly textured polycrystal. Minimization of
 196 the total energy $\Delta U_F + \Delta U_e$ yields an equilibrium top layer thickness $h^* = 1.01$ nm, or
 197 approximately five {111} layers, and a net energy change $\Delta U^* = -0.1547$ nJ/m. The
 198 minimum corresponds to elastic parameters along the GB normal and is close to that based on
 199 a polycrystalline average ($h^* = 1.00$ nm), see Tab. SM-5.

200 The continuum analysis is performed for a single crystal, and therefore ignores higher
 201 order corrections, if any, due to stress accommodation at the GB. Surface stresses and stress-
 202 dependent GB energies can drive additional changes. We capture these corrections using all-
 203 atom computations with rotated layer thickness in the range $0 \leq h \leq 2$ nm, or 0 –
 204 9 {111} layers. The variation in the total energy of the eGB system, also plotted in Fig. 4b for
 205 comparison, is similar to the continuum predictions with a slight shift in the minimum to $h^* =$
 206 1.25nm. The energy change $\Delta U^* = -0.0954$ nJ/m is smaller, likely due to the discrete nature
 207 of the {111} layers and stress-dependent bulk and interfacial parameters that are naturally
 208 incorporated in the atomistic model. This interplay is evident in the atomic stress distribution
 209 in Fig. 4e that exhibits a tensile to compressive stresses at the line defect that separates the two
 210 co-existing GBs, consistent with the elastic healing of a V-shaped notch (Fig. SM-11), and is
 211 distinct from the intrinsic stresses associated with each GB.

212 *eGB generalization to LAGB (energetics and subsurface structure)*

213 We test the generality of the energetic interplay at eGBs by performing a similar analysis
 214 for a valley formed at the eGB3.89 system (Fig. 5). A prescribed out-of-plane rotation of $\varphi =$
 215 1.375° corresponds to the [111] \rightarrow [112] shift of the misorientation axis (Tab. SM-1). The GB
 216 and surface contributions to the driving force together with FEM-based bulk elastic energy are
 217 plotted in Fig. 5a. The surface contribution for the LAGB is smaller, as expected. The net
 218 energy exhibits a minimum at $h^* \cong 13$ nm (Tab. SM-5) with negligible size effects at larger
 219 film thicknesses in the range $H = 50 - 100$ nm. MS computations of the eGB3.89 system
 220 around this minimum mimic the trends observed in the continuum computations, with an
 221 equilibrium rotated layer thickness that is shifted to $h^* = 14.4$ nm. The energy change of
 222 eGB3.89 system $\Delta U^* = -0.51$ nJ/m is again smaller than the continuum
 223 computations $\Delta U^* = -0.67$ nJ/m.

¹ Both contributions are dependent on the out-of-plane rotation φ , and therefore the misorientation angle θ ($\tan \varphi/2 \propto \sin \theta/2$). For LAGBs, the driving force approaches $\Delta\gamma$ and the surface contribution becomes increasingly important for HAGBs.

224 The surface profile shows corrugation with $D_1 \cong 110$ pm and $D_2 \sim 40$ pm, similar to the
225 STM profiles in NC films with small deviations ~ 7.5 nm away from TJ (Fig. 5b). The
226 corrugation ~ 70 pm is indicative of dissociated partial dislocations. The surface TJ exhibits a
227 $1/2 [\bar{9}817]$ period vector and the SF ribbon planes lie on the CPP, consistent with $[112]$ tilt
228 axis. The elastic stresses due to the reorientation increase the width of the SF ribbons at the
229 surface (Fig. SM-13), suggestive of a GB contribution to the stress accommodation. Both
230 experimental and atomistic peak (X_2) profiles reveal additional reconstructions at the SF edges
231 at the surface that subvert the complete formation of the local groove. Figure 5c-d show the
232 subsurface structure of the LAGB and stress distribution around the eGB. We see a sharp
233 transition between the two co-existing GB structure, stabilized by a diffuse (compressive)
234 stress, and the transition from tensile to compression stresses occurs well away from the line
235 defect separating the two GB structures. The overall interplay between geometry and
236 mechanics is similar to the observations for eGB26. The excellent agreement between
237 atomistics and continuum computations for both eGBs indicates that higher order effects have
238 a minimal effect on the energetics that sets the thickness of the rotated layer.

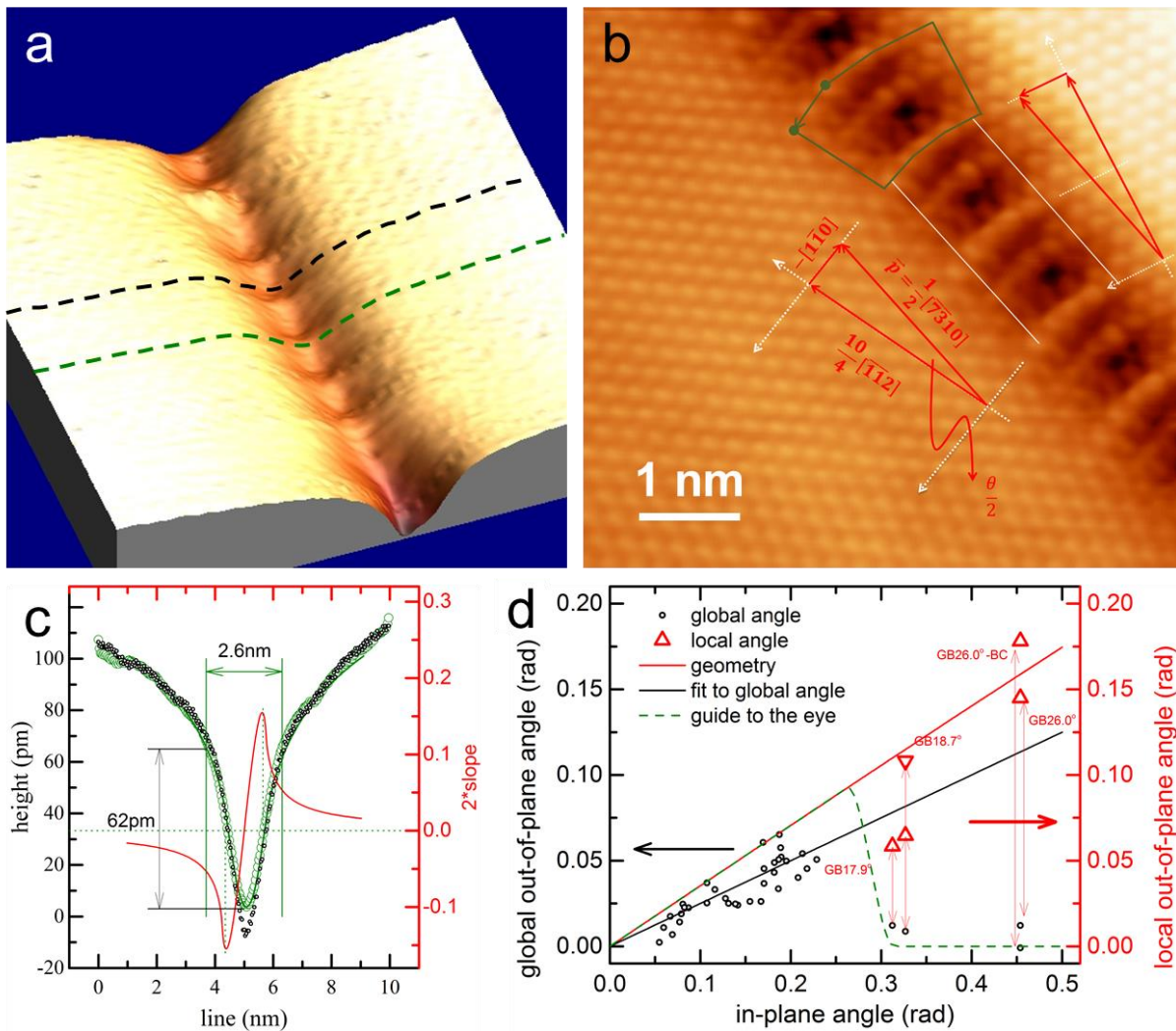
239 *Concluding remarks*

240 In this paper we demonstrated the existence of a natural driving force that restructures GBs
241 at surfaces. This phenomenon will be particularly important whenever there is an interplay
242 between GB energy, structure and stress. For example, tensile or compressive stresses
243 generated in films at different growth stage^{24,25} will modulate the intrinsic stress of eGBs,
244 decreasing (increasing) the length scale at valley-shaped (ridge-shaped) boundaries,
245 respectively. It will also impact material properties controlled by GBs, particularly in ultrathin
246 films with thicknesses approaching the length scale of the restructured boundary and stress
247 fields. In this instance, the film is comprised of a network of restructured boundaries and the
248 surface effect described here becomes a size effect. Since $[112]$ lies within a CPP, any
249 boundary with this tilt axis can be considered to be a folded CPP. Given that electronic
250 transport in copper occurs predominantly along CPPs^{11,26,27} these $[112]$ boundaries should
251 exhibit reduced levels of boundary scattering. To realise these benefits it is necessary to
252 develop processes that enable the deposition of materials with thermodynamically-relaxed
253 $[112]$ tilt boundaries.

254 J.J.B and X.Z. acknowledge support from Science Foundation Ireland grants
255 (12/RC/2278 and 16/IA/4462) and early discussions with David Srolovitz, Adrian Sutton and
256 Jian Han, and thank Peter Gleeson and John J. Plombon from Intel Corporation for the PVD
257 samples. H.W. and M.W. acknowledge support from the National Natural Science Foundation
258 of China (Grant No. 12172347) and the Fundamental Research Funds for the Central
259 Universities (Grant No. WK2480000006).

260 **Figure 1 Grain boundary structures at atomic resolution and nanoscale.**

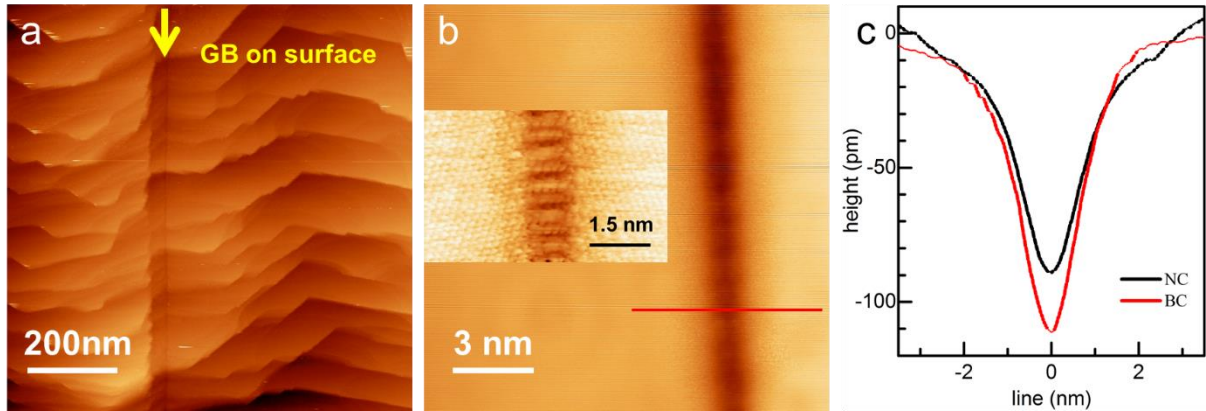
261 (a) Perspective view of GB 26.01°. (b) atomic resolution mapping of GB 26.01°. The red lines
 262 show the vectors in both half crystals. The green path shows a Burgers circuit with a closure
 263 failure of a content two times nearest-neighbor distance. (c) STM topography of GB 26.01°. (d)
 264 Data points of white and green lines in (c). The black line is a local fit of the green points
 265 and the red line is the first derivative of the black line. Tunneling parameters for (a) are $I = 20$
 266 pA and $U = -500$ mV. Tunneling parameters for (b) are $I = 30$ pA and $U = 5$ mV. (d) The local
 267 and global out-of-plane angles as a function of in-plane angles for LAGBs and HAGBs. Note
 268 that GB [111] 18.74° shows a range of the out-of-plane displacement angles at different sites.



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 270

271 **Figure 2 Grain boundary structure at surface in bicrystal.**

272 (a) STM topography image shows a straight line, where GB 26.01° emerges at the bicrystal
 273 (BC) surface. (b) STM image of eGB26 at the surface. Inset, shows atomic resolution of the TJ
 274 region and confirms the $[3,2,3,2]$ decomposition. (c) Topographic profile of the TJ groove
 275 recorded along the cross section in (b) together with the profile of the TJ groove at the
 276 nanocrystalline (NC) surface. Tunneling parameters for (a) are $I = 20$ pA and $U = 2$ V, for (b)
 277 inset are $I = 20$ pA and $U = 20$ mV, for (b) are $I = 20$ pA and $U = -200$ mV.

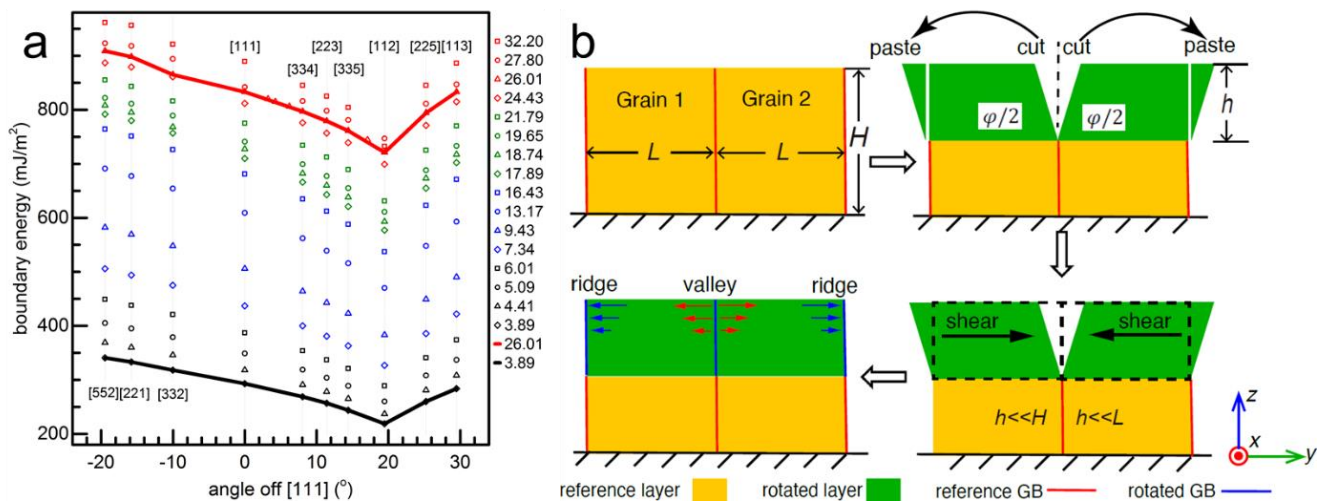


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280 **Figure 3 GB energy and eGB calculation.**

281 (a) In-plane angle dependent GB energy as the composite axis shift from $[111]$ to $[112]$ through
 282 out-of-plane rotation. (b) Computational scheme used to study the partial rotation of a top layer
 283 of thickness h (shaded green) within a film of thickness $H \gg h$. Solid lines indicate GBs
 284 separated by the grain size L . Red and blue lines correspond to the unrotated and rotated GBs,
 285 respectively. The location of the valleys and ridges are as indicated.

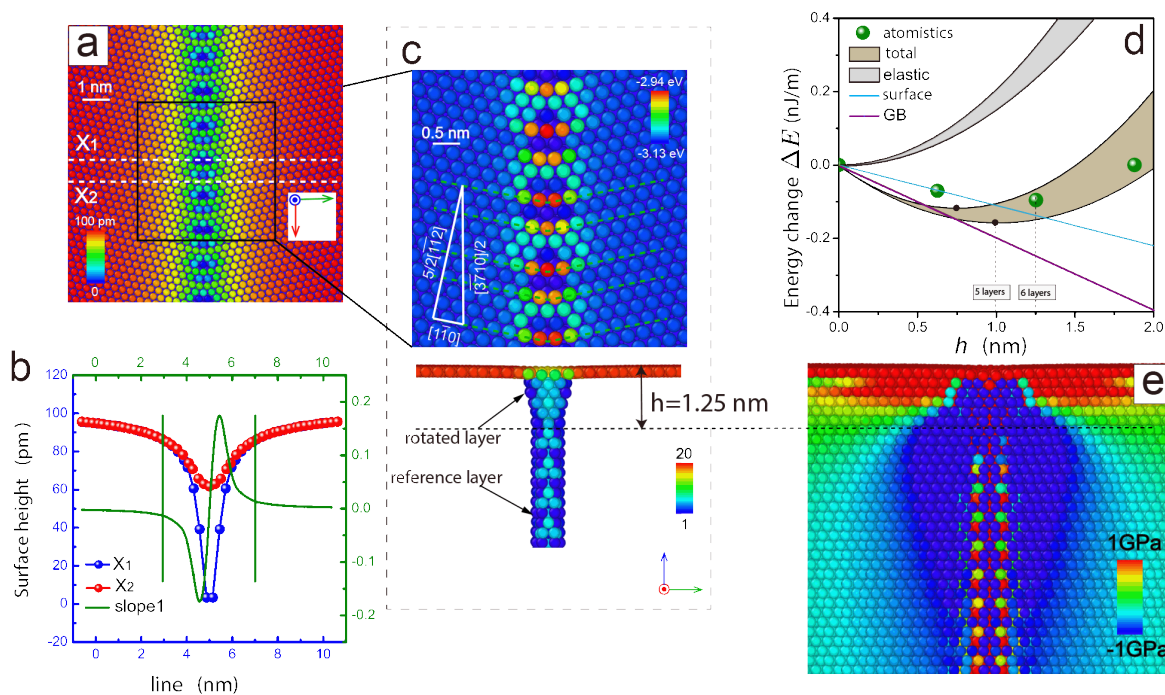


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288 **Figure 4 Structure, morphology, and mechanics of the eGB26 system.**

289 (a) Atomic-scale configuration of an equilibrated eGB composed of the $\theta = 26.01^\circ$ HAGB
 290 with a rotated layer thickness of 1.25 nm, or 6 $\{111\}$ layers in a $H = 50$ thick $\{111\}$ copper
 291 film. Atoms are coloured based on their depth coordinate. (b) Line profiles along troughs (blue,
 292 X_1) and peaks (red, X_2) within the undulating surface TJ, as indicated in (a). The solid green
 293 line is the slope of the X_1 profile. (c, top) Magnified view of the surface TJ. The dashed green
 294 lines connecting close-packed directions across the eGB serve as guides for the planar
 295 decomposition of the indicated periodicity vector. Atoms are coloured based on the potential
 296 energy (c, bottom). Side view showing the through thickness GB structure within the rotated
 297 and reference layer. The defect atoms are identified and coloured based on the central
 298 symmetry parameter. (d) The GB, surface and elastic energy contributions to the total energy
 299 of the eGB for varying rotated layer thicknesses. The elastic energy cost is plotted as a range
 300 based on continuum (FEM) computations; see text for details. Green spheres are results of MS
 301 simulations. The minima corresponding to the continuum and atomistic plots are indicated. (e)
 302 Through-thickness stress distribution in the vicinity of the eGB. The color indicates the atomic
 303 (virial) stress.

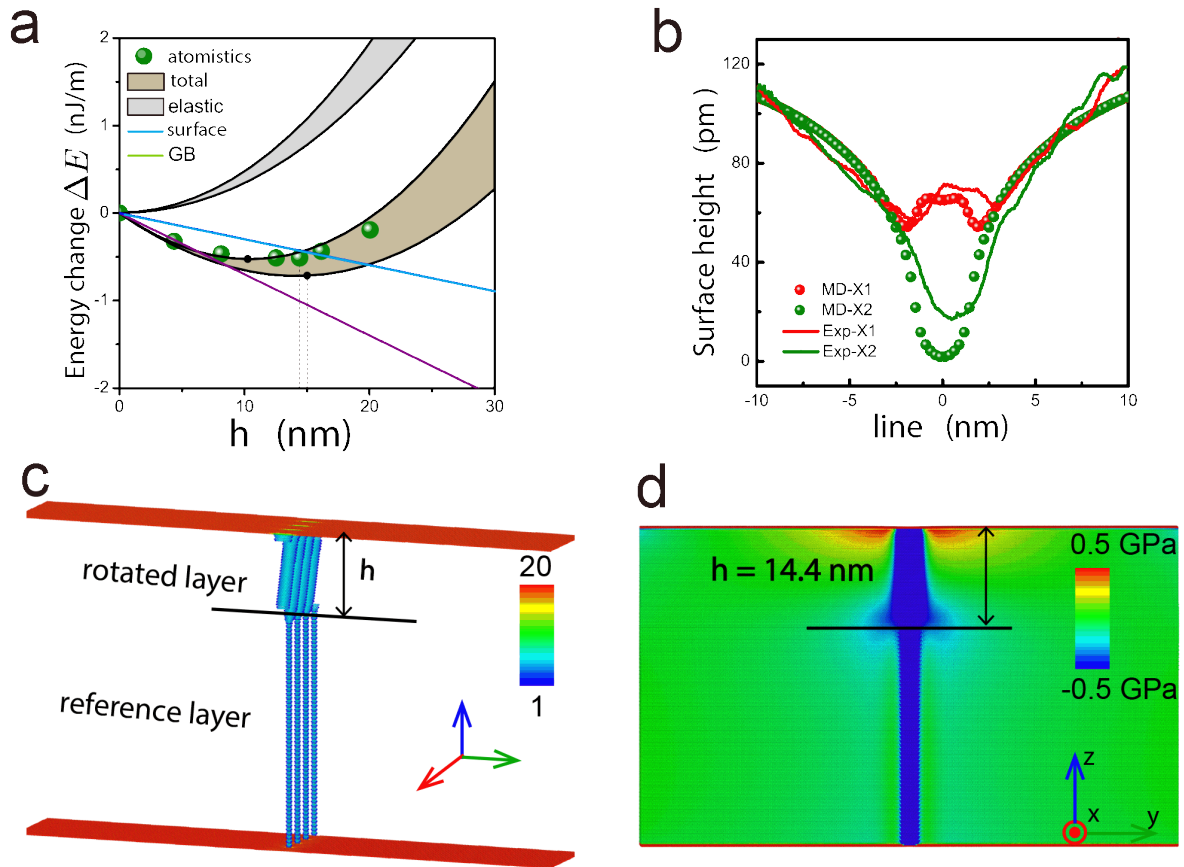


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306 **Figure 5 Atomistic-continuum computational analyses for the eGB3.9 system.**

307 (a) Same as in Fig. 4d, but for eGB composed of the $\theta = 3.89^\circ$ LAGB. The vertical dashed
 308 lines indicate the minima for the continuum and atomistic computations. (b) The trough (green)
 309 and peak (red) line profiles extracted via MS simulations (spheres) and STM characterization
 310 of a 50 nm thick NC copper film (solid lines). (c-d) Through thickness (c) GB structure using
 311 the central symmetry parameter and (d) stress distribution based on the atomic stress observed.



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